#### **Mixed-material studies in PISCES-B**

R. Doerner for the PISCES Research Team Part of the US-EU collaboration on Mixed-Material Effects on ITER

- Introduction
- Technical results
  - Temporal behavior of chemical erosion suppression
  - Response of Be/C to thermal transients
- Summary of possible mixed-material implications for ITER





#### PISCES-B has been modified to allow exposure of samples to Be seeded plasma





## Erosion suppression exhibits a temporal evolution ( $\tau_{Be/C}$ )



- Understanding the temporal behavior is critical to determining the fundamental mechanisms responsible for erosion mitigation
- PMI modeling codes should be able to reproduce temporal behavior to provide confidence





# XPS data shows Be<sub>2</sub>C formation in resultant mixed-material surface

XPS analysis of Be on C sample surface [M. Baldwin et al., in press JNM]



- Virtually all C remaining at the surface is bound as carbide (t >  $\tau_{Be/C}$ )
- Presence of carbide inhibits chemical erosion of C
- Carbide layer reduces sputtering yield of bound Be
- Subsequently deposited Be can be more easily eroded
- Codeposits are primarily Be once carbide layer forms





#### If Be acts like B doping, then Be should inhibit C atoms from chemically eroding



- Chemical erosion model [Schenk et al. JNM 220-222(1995)767] predicts boron reduces sp<sup>2</sup> component in favor of sp<sup>3</sup> hybridization.
- In-situ Be seeding data shows similar behavior of chemical erosion mitigation





#### Be first shuts down C chemical erosion, then subsequent Be re-erodes from surface



- Evolution of a mixed Be/C surface
  - Be oven opens at t = 0 sec.
  - Be ions arriving at t < 50s shut down chemical erosion by forming Be<sub>2</sub>C surface layer [Baldwin JNM 2006 available on-line]
  - Once Be<sub>2</sub>C is formed, subsequent Be arriving (T > 50 s) is more easily eroded and begins coating windows
  - Be<sub>2</sub>C surface thickness saturates after carbide forms 50s in this exposure [Baldwin JNM 2006]
  - Resultant codeposited material is primarily Be [Baldwin JNM 337-339(2005)590]





# WPM samples show collection of beryllium-rich codeposits during Be seeding runs



More C is detected in codeposits during lower C target temperature exposure (possibly due to a combination of lower chemical erosion yield and/or quicker beryllium carbide layer formation)



Chemical erosion suppression time  $(\tau_{Be/C})$  depends on several quantities that can be varied almost independently







# PISCES chemical erosion mitigation time scaling predicts suppression between ELMs in ITER

 $\tau_{\text{Be/C}}^{\text{scale}}[s] = 1.0 \times 10^{-7} c_{\text{Be}}^{-1.9 \pm 0.1} E_i^{0.9 \pm 0.3} \Gamma_i^{-0.6 \pm 0.3} \exp(((4.8 \pm 0.5) \times 10^3 / T_s))$ 



- Surface temperature effects reaction rate
- Be plasma concentration effects arrival rate at surface
- Ion energy effects erosion rate
- Ion flux impacts through redeposition
- Type of graphite does not seem to play a significant role (ATJ vs. CFC)
- Scaling law using these variables has been developed to allow extrapolation to ITER conditions ( $\tau_{Be/C}^{ITER} \sim 6$  msec) [ $c_{Be} = 0.05, E_i = 20$  eV,  $T_s = 1200$  K and  $\Gamma_i = 10^{23}$  m<sup>-2</sup>s<sup>-1</sup>]





#### Thermal transient experiments: Motivation for positive pulse biasing

- PISCES has shown that Be plasma impurities suppress carbon target erosion at temperatures up to 1000°C
- ITER will experience large temperature excursions (up to 3800°C) at the carbon dump plates during periodic ELMs
- Will the thin, surface Be, Be/C layers survive such dramatic temperature excursions?
- How will Be-W react during temperature excursions?
- It is possible to simulate the large temperature excursions associated with ITER ELMs in PISCES-B using positive sample biasing during plasma discharges.





# Large power loads can be drawn to P-B sample during positive biasing



- During 1.5 MW/m<sup>2</sup> power pulse graphite surface temperature rises to ~2000°C (by pyrometers)
- Bulk graphite temperature rise at back of sample ~20°C during 0.1 s. pulse (thermocouple)
- Surface temperature rise is limited by power supplies (IPP has supplied a new power supply as part of US-EU collaboration)





### Transient surface heating promotes $Be_2C$ formation leading to shorter mitigation times



Surface temperature during heat pulse ~ 1200°C [from R. Pungo et al., PSI17]

- Pulsing surface temperature to the 1200°C range results in faster chemical erosion suppression
  - Be<sub>2</sub>C disassociates at ~2200°C at 1 atm
  - Beryllium boiling point = 2471°C at 1 atm
- D retention during transient surface heating also increases by ~50% both with and without Be plasma seeding





#### How might mixed materials impact ITER?



- Due to elevated temperature of C dump plates, carbides will likely form and limit C erosion
- If a full C divertor were employed, carbide formation on regions of the baffles, where the temperature is lower, would take longer, resulting in more C erosion and thereby more hard-to-remove tritium
- Be deposition on W baffles will likely not result in significant beryllide formation  $(T_W \sim 400^{\circ}C)$
- If a full W divertor were used, beryllide formation near the strike points would be a concern (perhaps an issue for the JET ITER-like wall experiments)
- Beryllide formation in ITER only appears to be a concern on the W cassette liner 'louvers' (that are designed to be hot surfaces)



